

COUPLED THCM MODELS OF HEATING AND HYDRATION TESTS TO STUDY THE INTERACTIONS OF FE CORROSION PRODUCTS AND BENTONITE

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1. INTRODUCTION

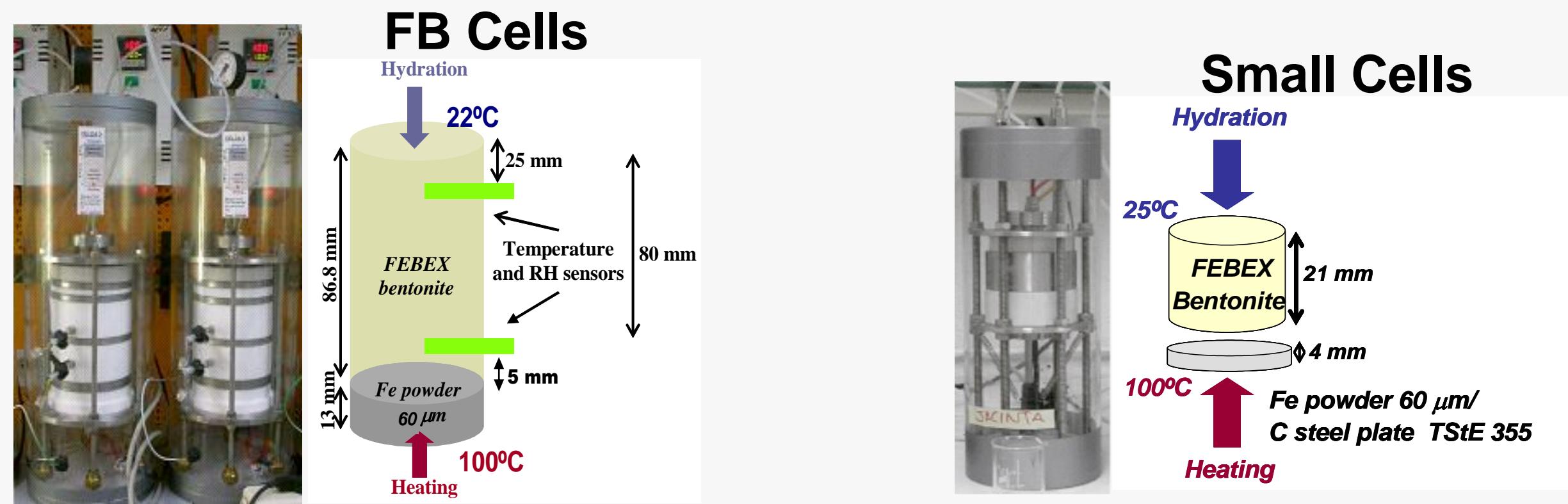
- Compacted bentonite is foreseen as a backfill and sealing material in radioactive waste repositories
- The strong interplays among thermal (T), hydrodynamic (H), mechanical (M) and chemical (C) processes during the hydration and thermal stages of a repository call for coupled THMC models.
- Many laboratory experiments have been performed on canister corrosion, corrosion-bentonite interactions and concrete-bentonite interactions.
- There is a clear need to test the models used in performance assessment analyses with laboratory data.

2. OBJECTIVES

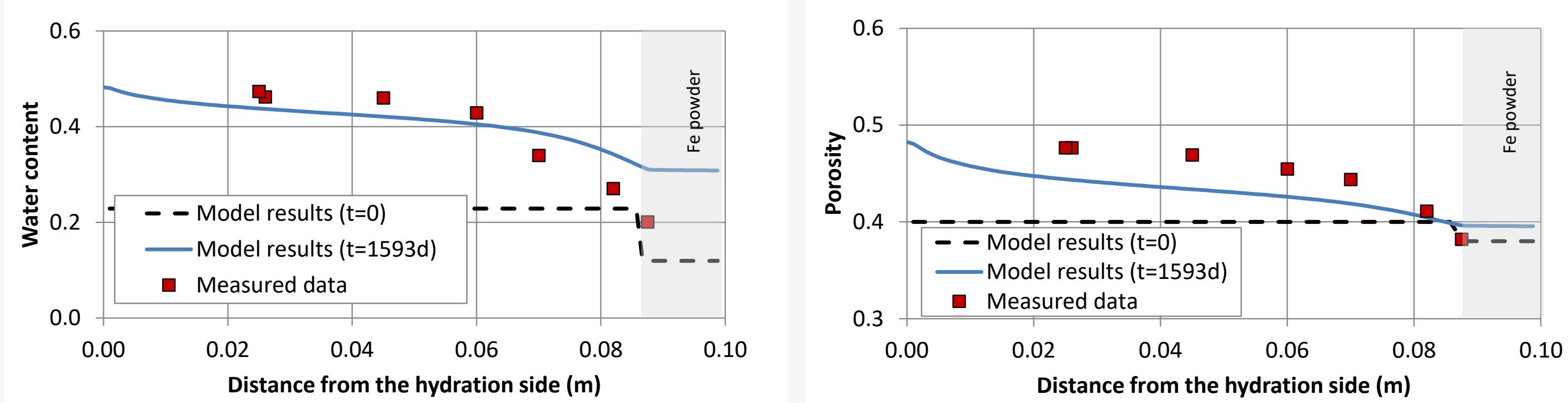
- We present coupled THMC models of heating and hydration corrosion experiments performed at the Ciemat facilities to study the corrosion products generated at the canister/bentonite interface under repository conditions and analyze how the corrosion products could affect bentonite properties

3. HEATING & HYDRATION CORROSION TESTS

- Some of these experiments were performed within the NF-PRO and PEBS Projects (ENRESA, 2008, Turrero et al., 2011) while others are being dismantling within EURAD Project.

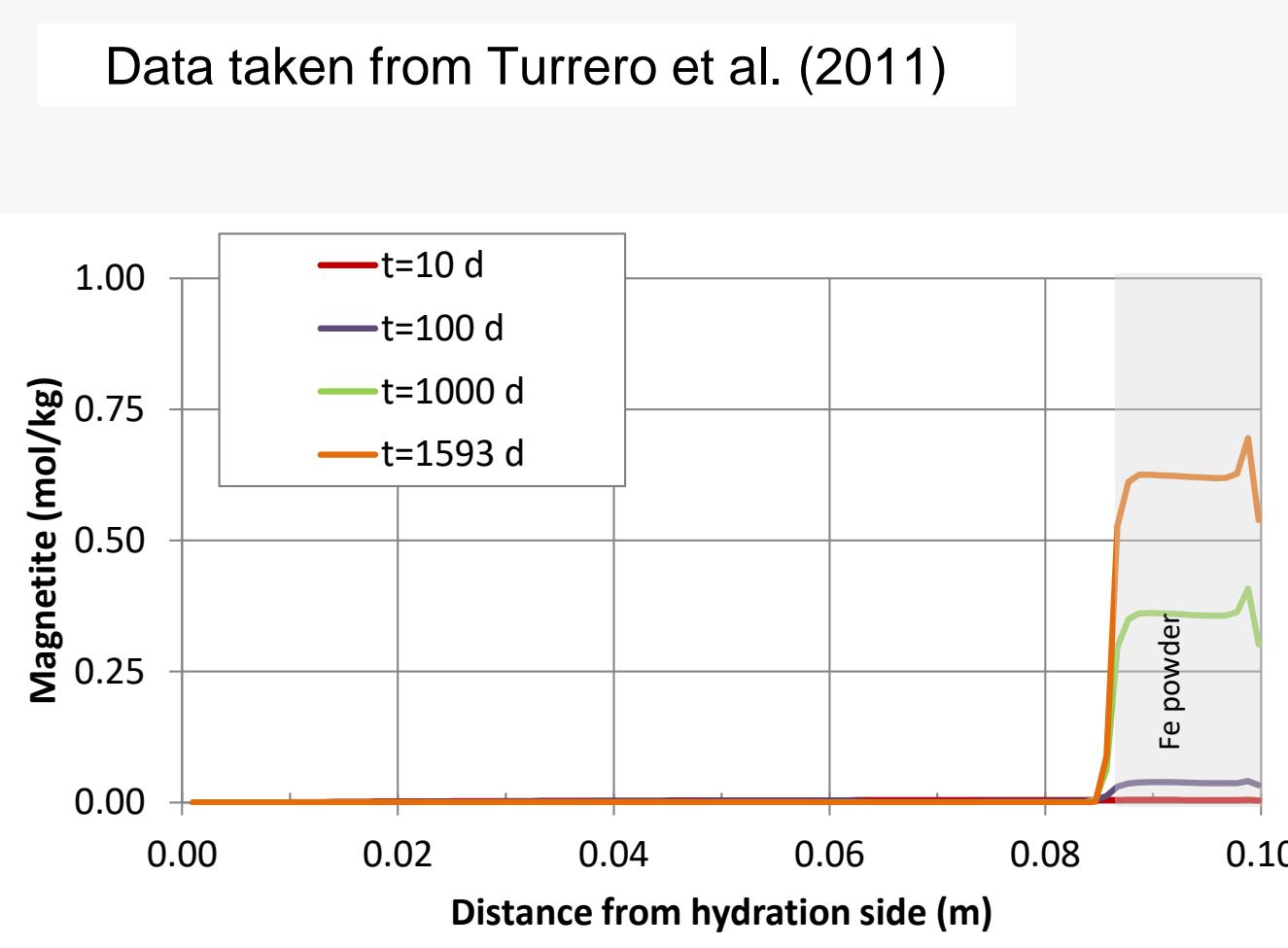


5. NUMERICAL MODEL RESULTS OF FB3 CELL



MAJOR FINDINGS

- Model results predict a small amount of magnetite precipitation computed at the bentonite/Fe powder interface which is consistent with magnetite precipitation observed at the interface.
- The precipitation of magnetite at chemical equilibrium is larger than that computed with a kinetically-controlled precipitation.
- $\text{Fe(OH)}_2(s)$ does not precipitate when magnetite precipitates at equilibrium and when the corrosion rate is decreased.

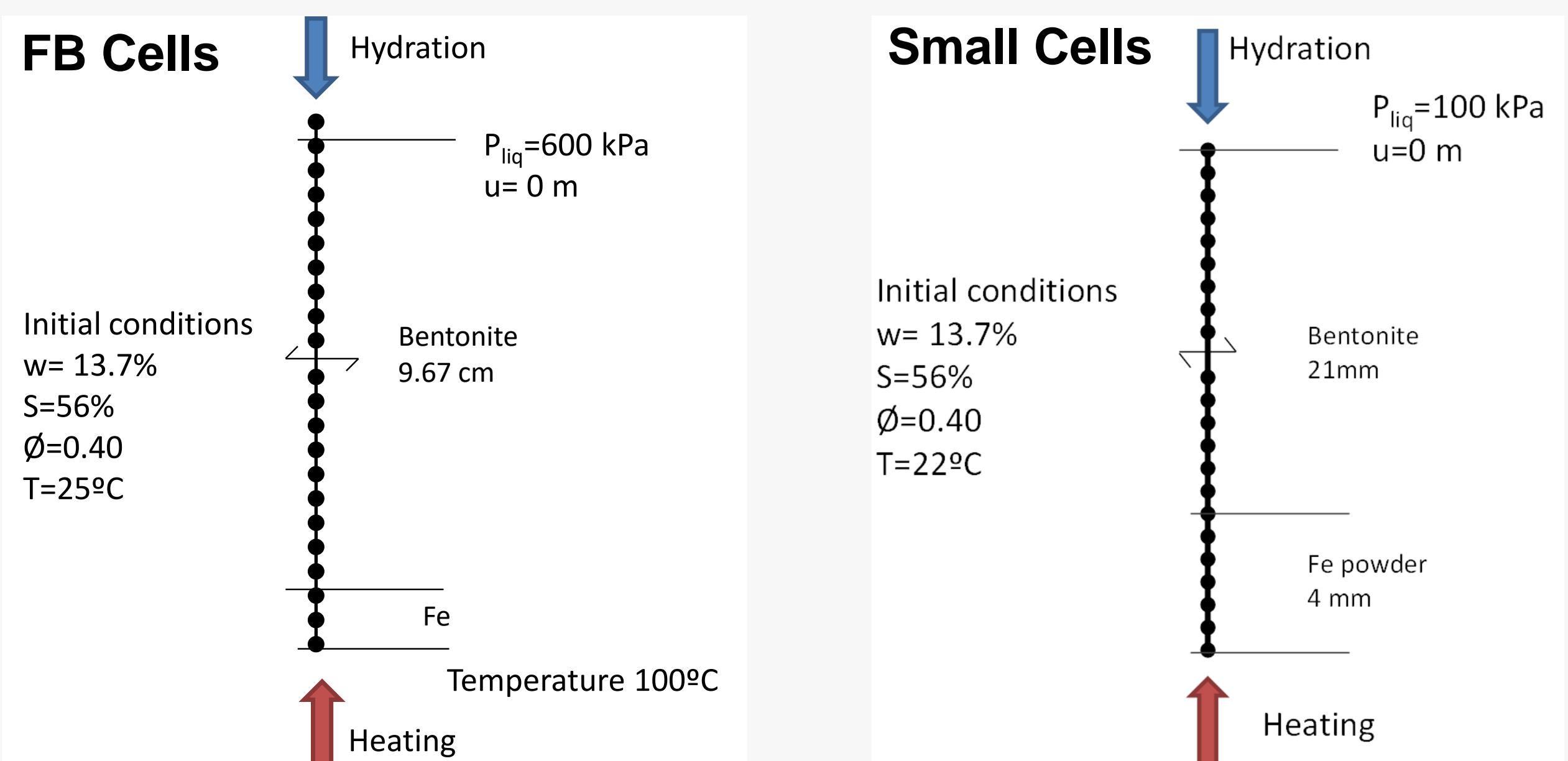


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4. THCM MODEL OF CORROSION EXPERIMENTS

- 1D finite element grid
- A temperature of 100°C is imposed at the heating boundary
- THMC parameters were taken from Zheng et al. (2010)
- The numerical model was performed with INVERSE-FADES-CORE (Zheng et al., 2011; Mon, 2017) a code which solves multiphase flow and multicomponent reactive transport problems in deformable porous media

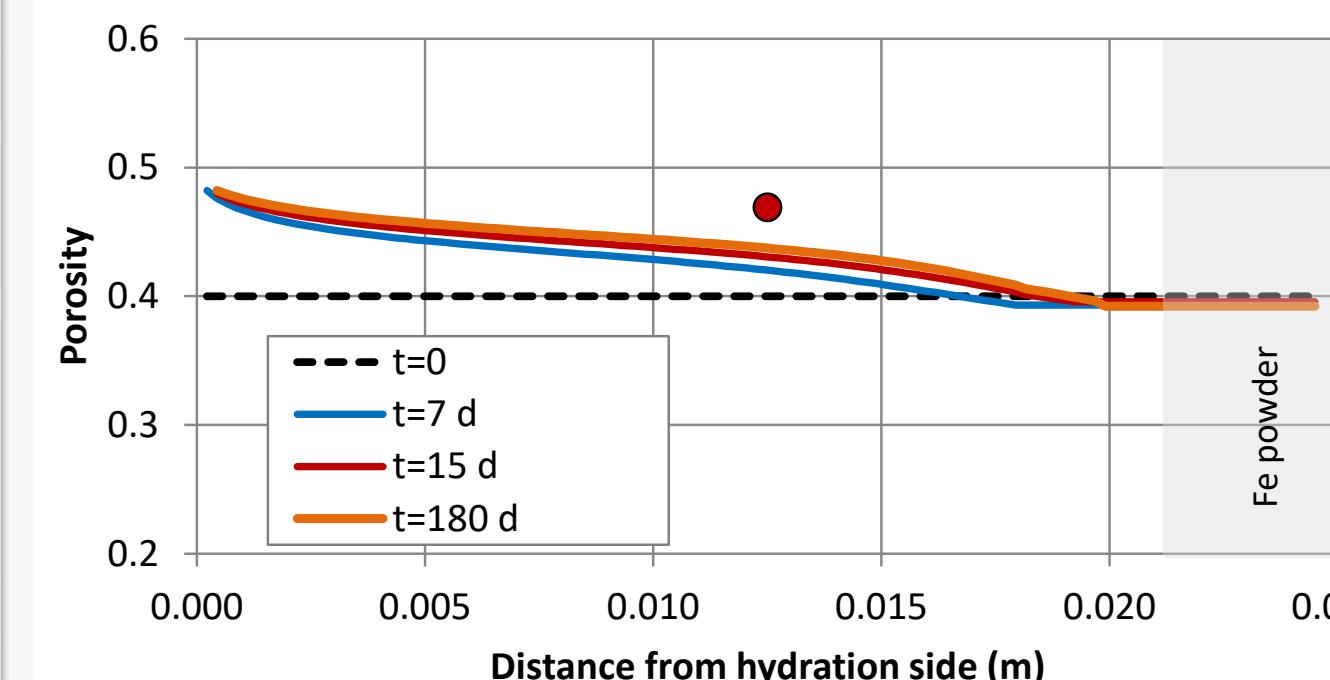


Geochemical system

Primary species	$\text{H}_2\text{O}, \text{H}^+, \text{Ca}^{2+}, \text{Mg}^{2+}, \text{Na}^+, \text{K}^+, \text{Cl}^-, \text{SO}_4^{2-}, \text{HCO}_3^-, \text{SiO}_2(\text{aq}), \text{O}_2(\text{aq}), \text{Fe}^{2+}$
Aqueous complexes	$\text{CaCO}_3(\text{aq}), \text{CaHCO}_3^+, \text{CaOH}^+, \text{CaSO}_4(\text{aq}), \text{CO}_2(\text{aq}), \text{CO}_3^{2-}, \text{KSO}_4^-, \text{MgCO}_3(\text{aq}), \text{MgHCO}_3^+, \text{MgSO}_4(\text{aq}), \text{MgOH}^+, \text{NaHCO}_3(\text{aq}), \text{NaSO}_4^-, \text{NaCO}_3^-, \text{NaOH}(\text{aq}), \text{OH}^-, \text{H}_3\text{SiO}_4^-, \text{HSO}_4^-, \text{HS}^-, \text{Fe}^{3+}, \text{FeHCO}_3^+, \text{FeCO}_3^-, \text{FeCl}^+, \text{FeCl}_2^+, \text{FeOH}^-, \text{FeOH}_2^+, \text{Fe(OH)}_3(\text{aq}), \text{Fe(OH)}_2(\text{aq}), \text{Fe(OH)}_4^-, \text{Fe(OH)}_2^+, \text{Fe(SO}_4)_2^-, \text{FeSO}_4(\text{aq}), \text{FeHSO}_4^{2-}, \text{Fe(OH)}_2^{4-}, \text{KOH}(\text{aq}), \text{H}_2(\text{aq}), \text{NaHSiO}_3(\text{aq}), \text{HSiO}_3^-, \text{Mg}_3\text{SiO}_4^+$
Minerals	calcite, quartz, gypsum/anhydrite, magnetite, siderite, goethite, $\text{Fe}(s)$, $\text{Fe(OH)}_2(s)$
Exchangeable cations	$\text{Ca}^{2+}, \text{Mg}^{2+}, \text{Na}^+, \text{K}^+, \text{Fe}^{2+}$

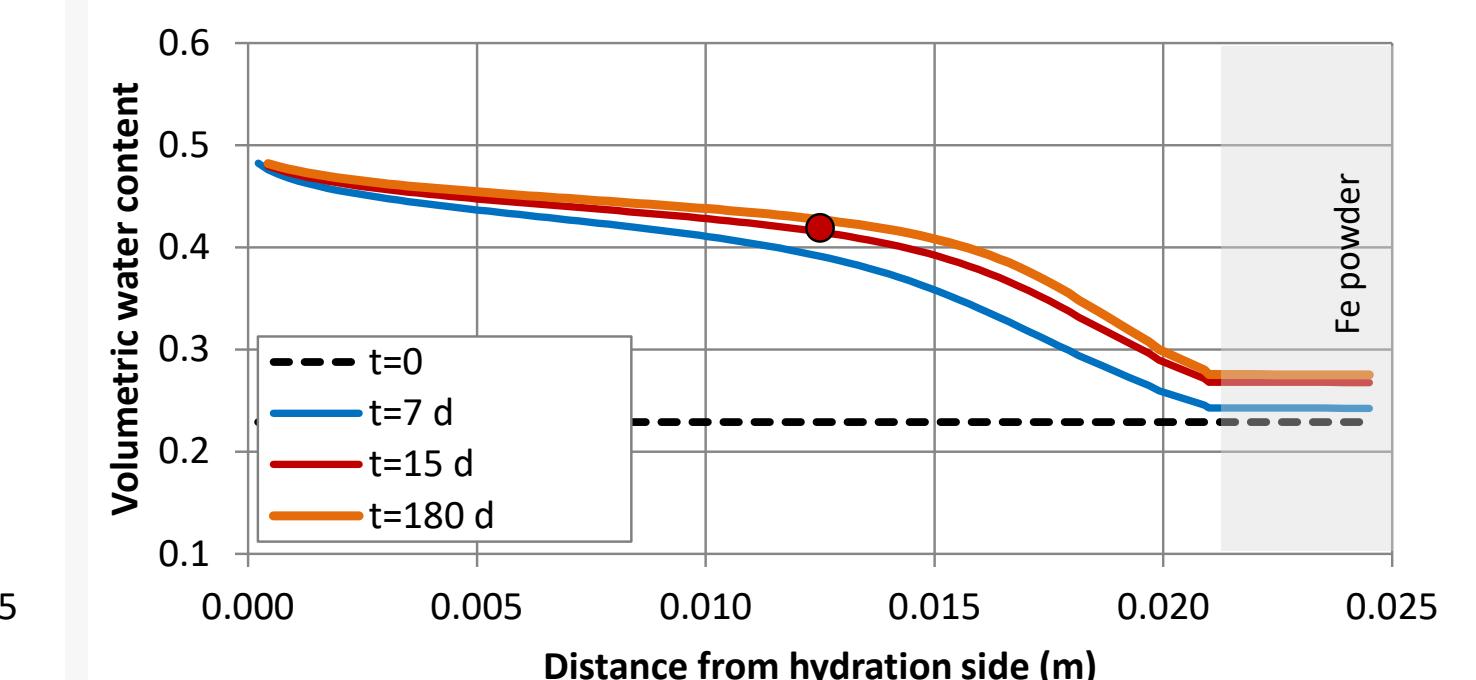
Cation exchange	$K_{\text{Na-cation}}$
$\text{Na}^+ + \text{X-X} \rightleftharpoons \text{K}^+ + \text{X-Na}$	0.138
$\text{Na}^+ + 0.5\text{Ca-X}_2 \rightleftharpoons 0.5\text{Ca}^{2+} + \text{Na-X}$	0.292
$\text{Na}^+ + 0.5\text{Mg-X}_2 \rightleftharpoons 0.5\text{Mg}^{2+} + \text{Na-X}$	0.280
$\text{Na}^+ + 0.5\text{Fe-X}_2 \rightleftharpoons 0.5\text{Fe}^{2+} + \text{Na-X}$	0.5
$\text{Na}^+ + \text{X-H} \rightleftharpoons \text{H}^+ + \text{X-Na}$	$3.16 \cdot 10^{-5}$
Surface complexation	$\log K_{\text{int}}$
$\text{SOH}_2^+ \rightleftharpoons \text{SOH} + \text{H}^+$	-4.5
$\text{SO}^- + \text{H}^+ \rightleftharpoons \text{SOH}$	7.9
$\text{SOFeOH} + 2\text{H}^+ \rightleftharpoons \text{SOH} + \text{Fe}^{2+} + \text{H}_2\text{O}$	0.6
$\text{S}^{\circ}\text{OFeOH} + 2\text{H}^+ \rightleftharpoons \text{S}^{\circ}\text{OH} + \text{Fe}^{2+} + 2\text{H}_2\text{O}$	10.0
$\text{S}^{\circ}\text{OFe(OH)}_2^- + 3\text{H}^+ \rightleftharpoons \text{S}^{\circ}\text{OH} + \text{Fe}^{2+} + 2\text{H}_2\text{O}$	20.0
$\text{S}^{\text{W}1}\text{OH}_2^+ \rightleftharpoons \text{S}^{\text{W}1}\text{OH} + \text{H}^+$	-4.5
$\text{S}^{\text{W}1}\text{O}^- + \text{H}^+ \rightleftharpoons \text{S}^{\text{W}1}\text{OH}$	7.9
$\text{S}^{\text{W}2}\text{OH}_2^+ \rightleftharpoons \text{S}^{\text{W}2}\text{OH} + \text{H}^+$	-6.0
$\text{S}^{\text{W}2}\text{O}^- + \text{H}^+ \rightleftharpoons \text{S}^{\text{W}2}\text{OH}$	10.5
Steel canister corrosion	
$\text{Fe}(s) + 2\text{H}_2\text{O} \rightleftharpoons \text{Fe}^{2+} + 2\text{OH}^- + \text{H}_2(g)$	

6. NUMERICAL MODEL RESULTS OF SMALL CELLS

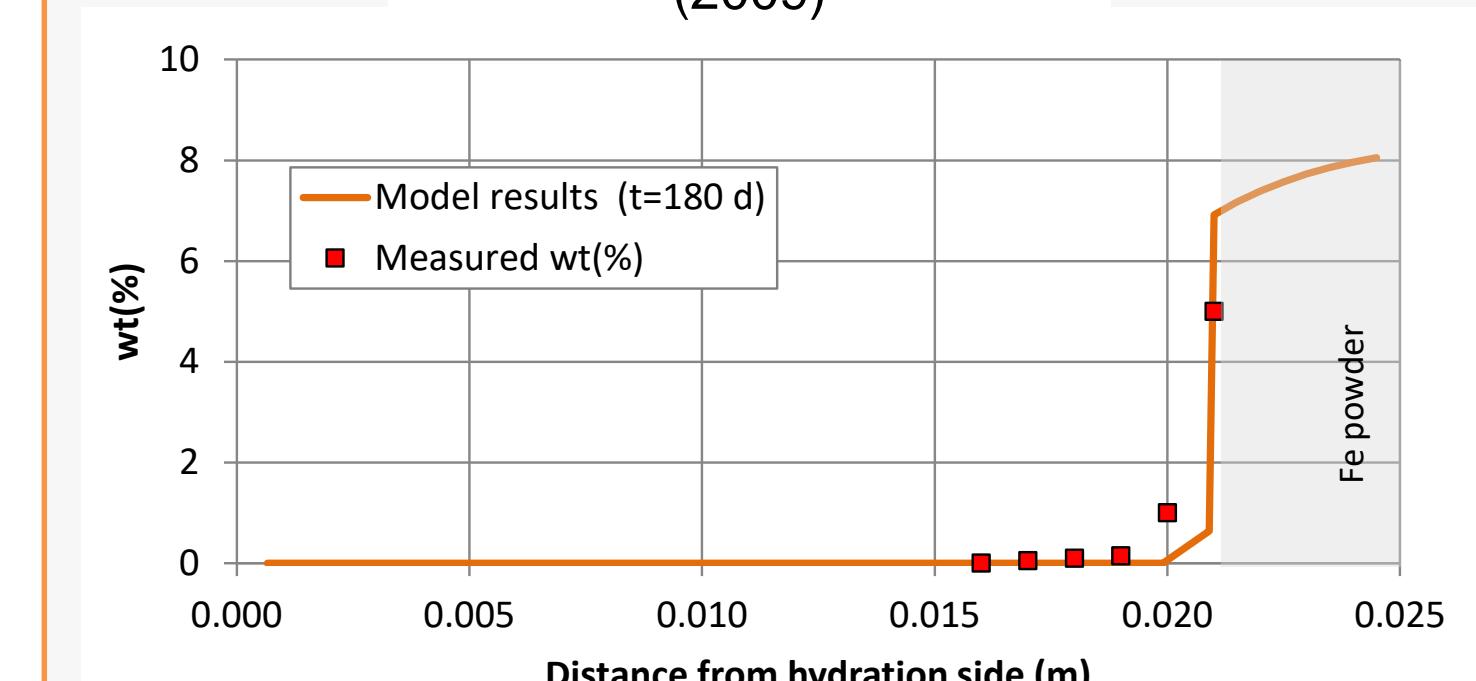


MAJOR FINDINGS

- Magnetite and $\text{Fe(OH)}_2(s)$ are the main corrosion products which compete for Fe^{2+} precipitation.
- The corrosion products penetrate a few mm into the bentonite.
- The numerical results fit the measured iron weight data.
- Fe^{2+} sorbs by surface complexation.
- Fe^{2+} exchange is less relevant than Fe^{2+} sorption by surface complexation.



Data taken from Torres et al. (2008) and De Windt et al. (2009)



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